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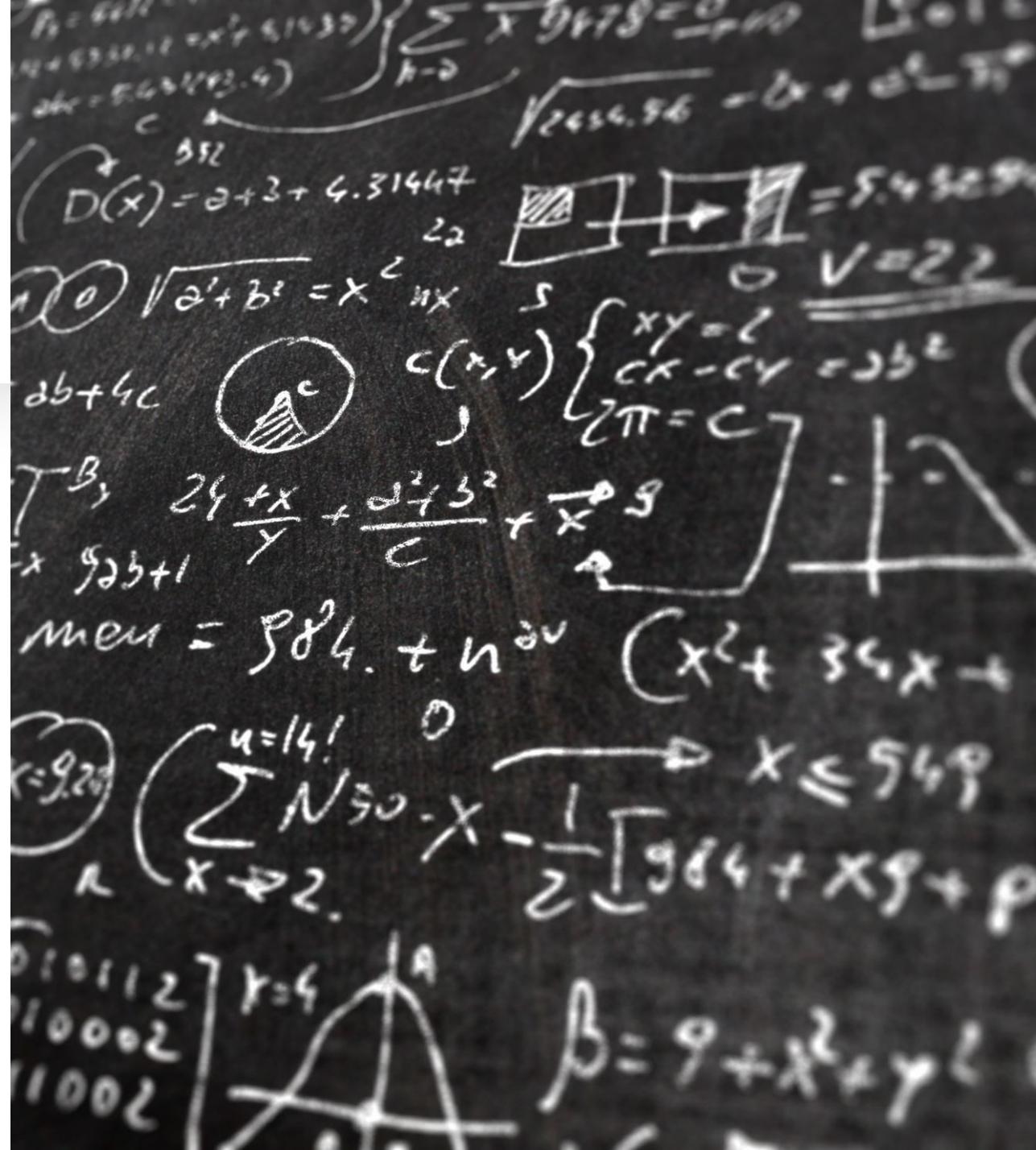
# An intuitive tour of parabolic reflector antennas

By K6MG

A large parabolic reflector antenna is shown in silhouette against a bright, orange and yellow sunset sky. The antenna is mounted on a complex metal structure with various beams and supports. The background shows a dark horizon line with some low hills or mountains. The overall scene is a dramatic, high-contrast image.

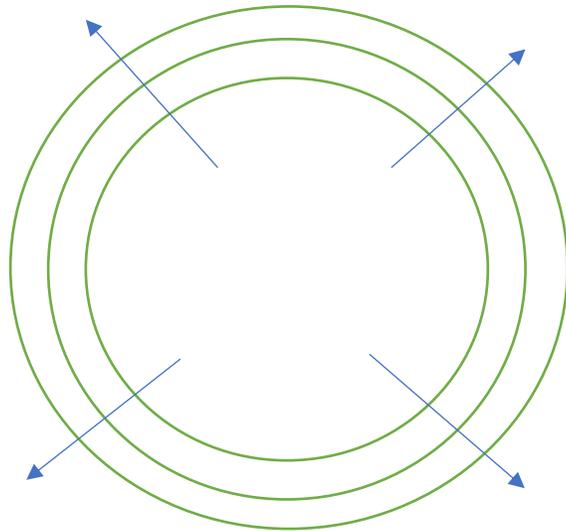
# Introduction

- No equations will be used in this presentation, however several equations were harmed in the preparation
- Why a parabola reflector ?
- The full parabola
- The offset parabola
- Multiple reflectors
- The ADE
- Reflectarray and Fresnel reflectors

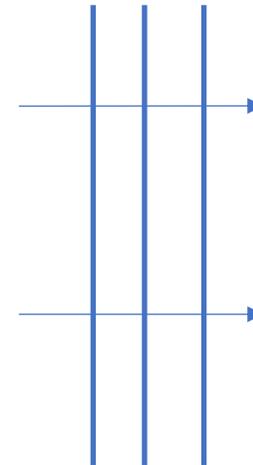


# Goal: directivity

Spherical wavefront



Planar wavefront

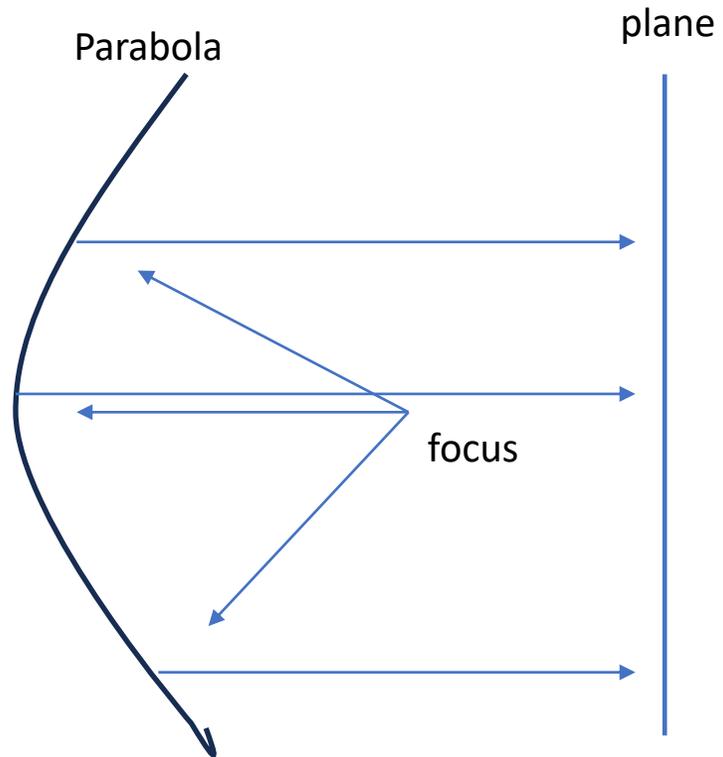


Wavefront: constant phase across the surface



Propagation through space and time

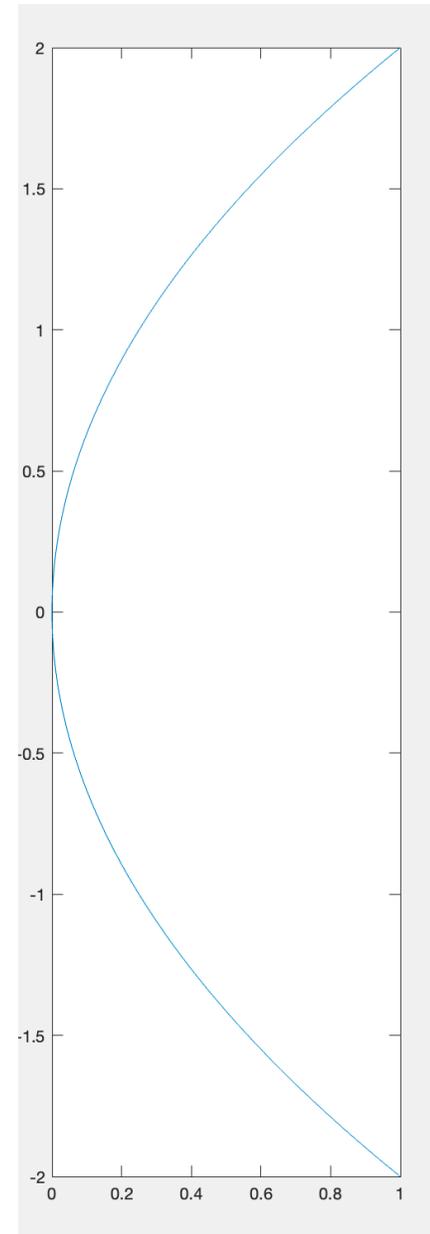
# Conversion from spherical to planar wavefronts



Constant distance from the focus to the plane at all angles

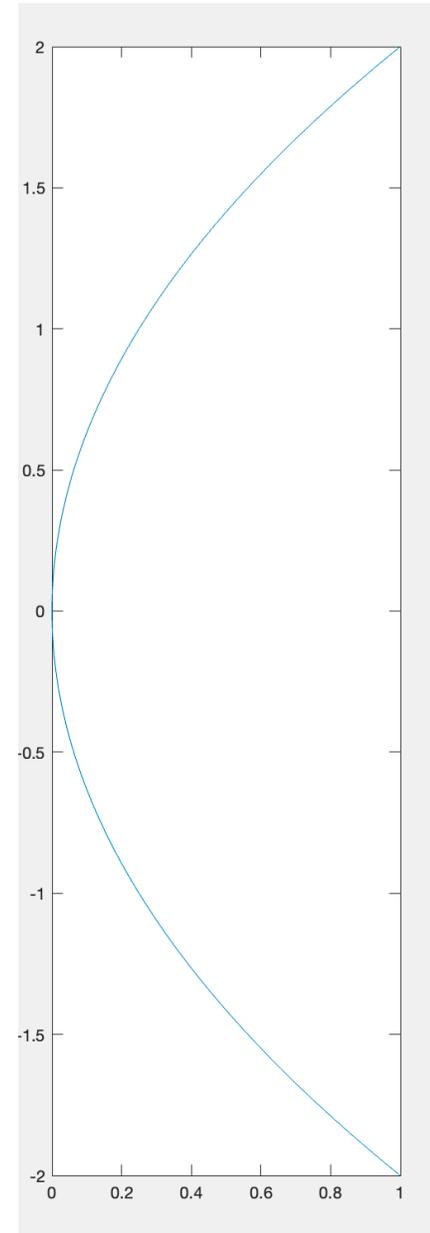
# Canonical full parabola

- Diameter 4 units
  - Focal length 1 unit
  - F/D 0.25
- 
- Were only interested in parabolas with  $F/D > 0.25$  since smaller  $F/D$  becomes too deep
- 
- Any parabola of interest can be made from this curve by truncating the diameter to get the desired  $F/D$  and scaling the units to the desired size



# Things to notice

- Truncating the diameter for higher F/D results in a “shallower” curve: the focus stays at the same place but the parabola edges pull back toward zero
- At 0.25 F/D the edges are in the same plane as the focus
- The angle of incidence == the angle of reflection, at 0 degrees the surface of the parabola is perpendicular to the wavefront, at 90 degrees the surface of the parabola is 45 degrees to the wavefront



# The offset parabola

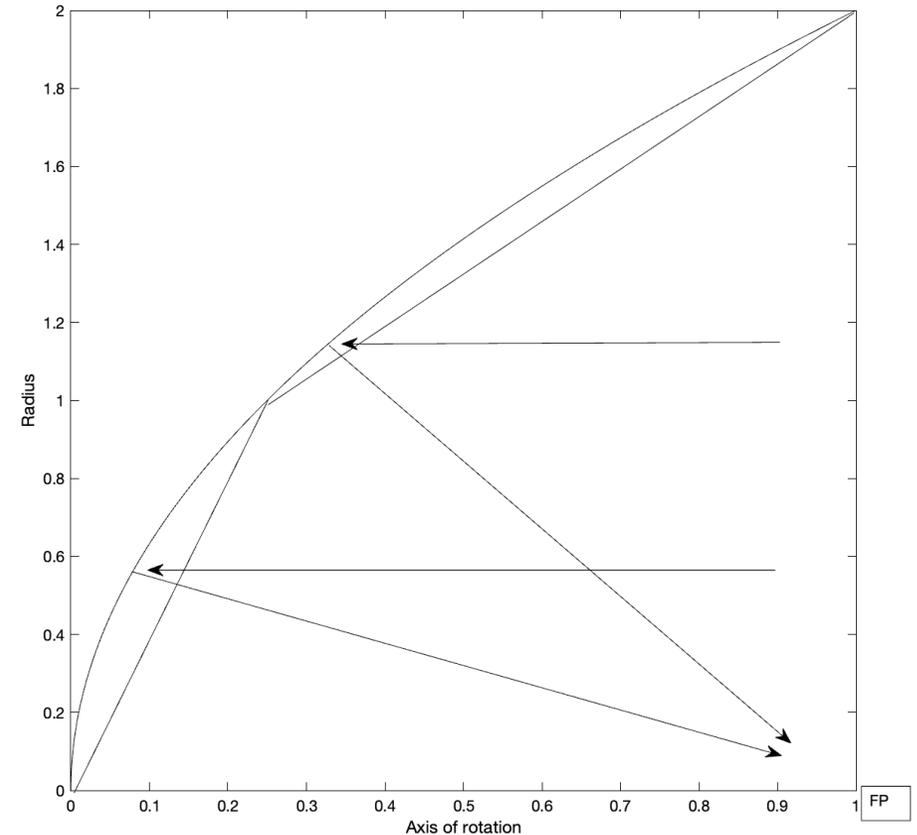
Uses at most half of the parabolic curve

The “offset” can be  $>0$  by starting the curve  $>0$

The focal length is defined as the distance from the lower edge of the curve to the focal point

The tilt angle is the angle from vertical of the plane across the edges

The “diameter” is defined as the aperture of the incoming/outgoing planar wavefront

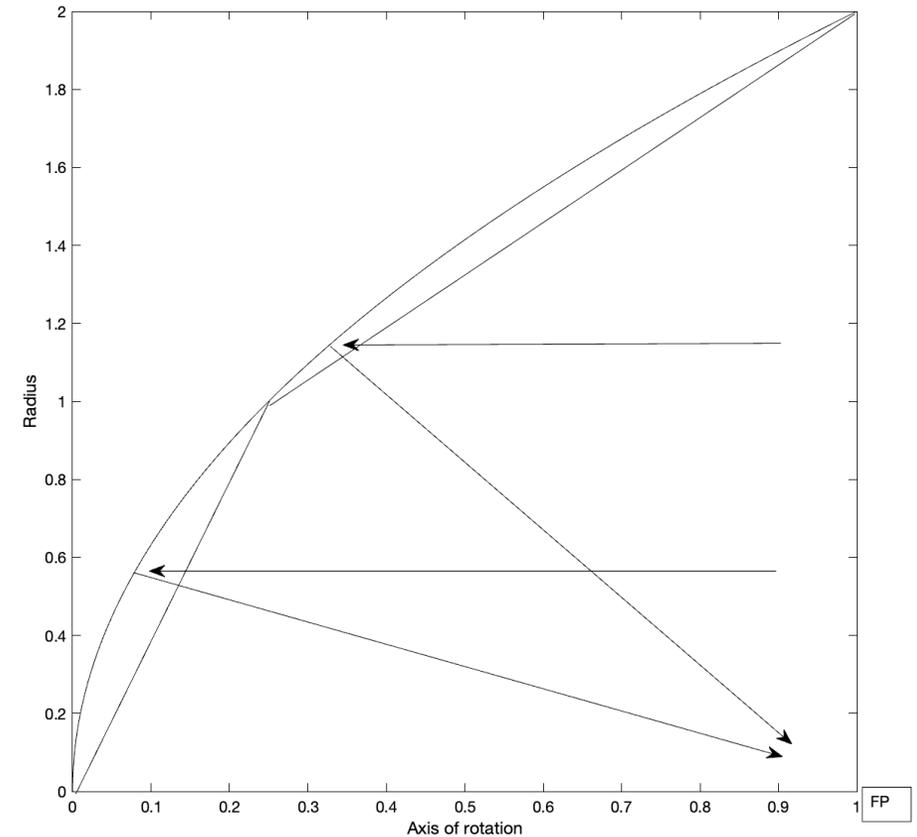


# Things to notice

The tilt angle is a function of  $F/D$  for any given offset, only one tilt angle is possible for an  $F/D$

Offsets  $>0$  require a larger segment of the curve to achieve the same aperture

A zero offset parabola has exactly double the  $F/D$  of the equivalent full parabola, the focal length is the same as the full parabola



# Offset tilt vs. F/D

| Tilt Angle | F/D  |
|------------|------|
| 14.5       | 1    |
| 15.25      | 0.95 |
| 16         | 0.9  |
| 17         | 0.85 |
| 18         | 0.8  |
| 19.25      | 0.75 |
| 20.8       | 0.7  |
| 22.6       | 0.65 |
| 24.5       | 0.6  |
| 27         | 0.55 |
| 30         | 0.5  |
|            |      |

# Inefficiencies



**Illumination** – nonconstant energy across the dish surface



**Spillover** – feed energy spills over the edge of the dish



**Blockage** – feed and supports block part of the aperture



**Ohmic** – reflective surface is not a perfect conductor



**Surface** – surface shape deviates from a perfect parabola



**Diffraction** – feed, supports and dish edges diffract some of the energy

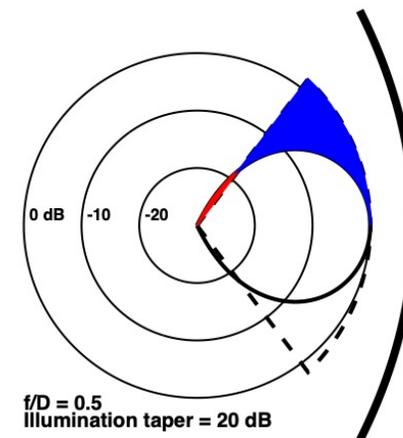
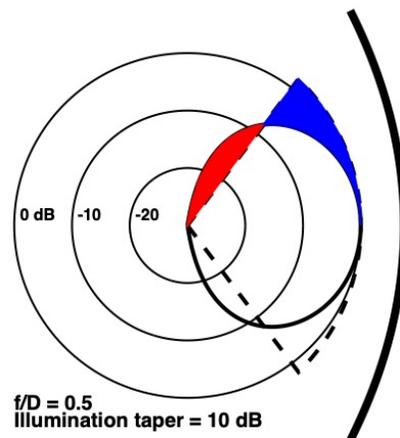
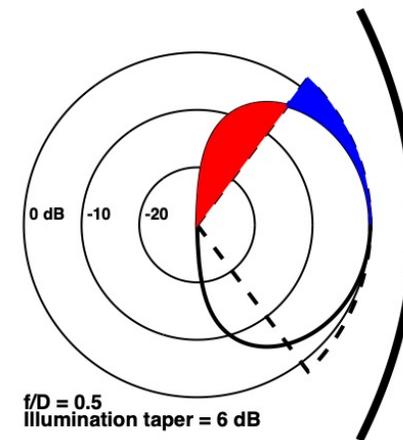
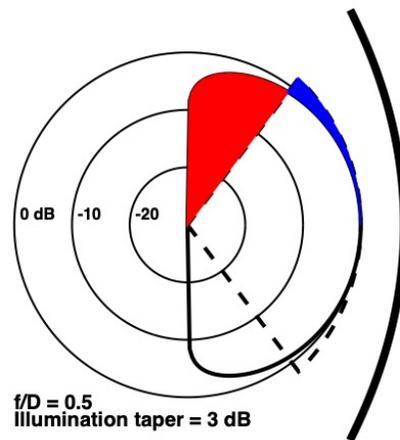


**Feedline** – energy loss between the radio and the feed

| Inefficiency | Prime focus | Offset  |
|--------------|-------------|---------|
| Illumination | 0.88        | 0.88    |
| Spillover    | 0.88        | 0.88    |
| Blockage     | 0.90        | 0.97    |
| Ohmic        | 0.99        | 0.99    |
| Surface      | 0.97        | 0.97    |
| Diffraction  | 0.95        | 0.98    |
| Feedline     | 0.90        | 0.98    |
|              | 57%         | 69%     |
|              | -2.4 db     | -1.6 db |

# Illumination and Spillover

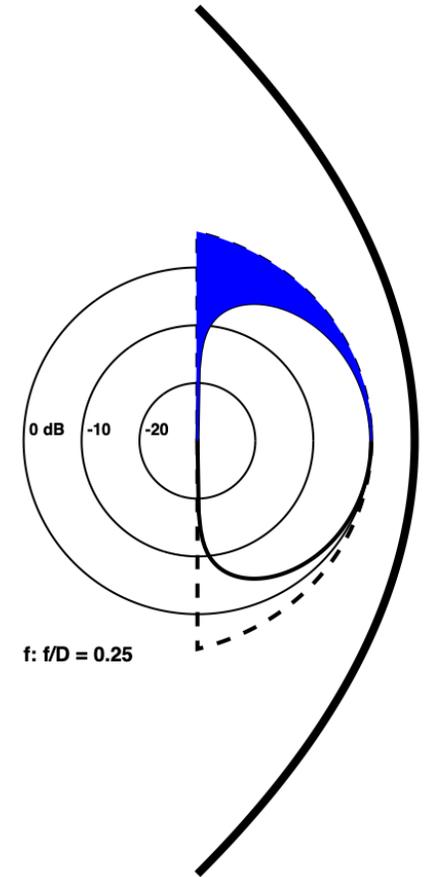
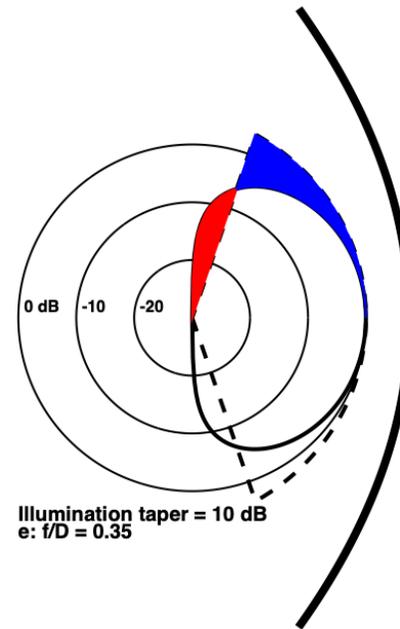
■ Illumination loss  
■ Spillover loss



# Illumination and Spillover

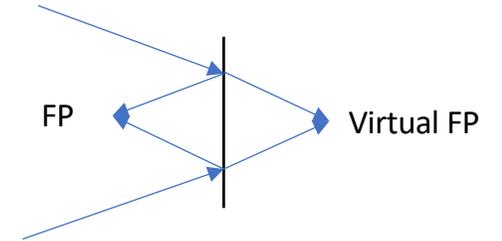
Illumination and Spil

- *Illumination loss*
- *Spillover loss*

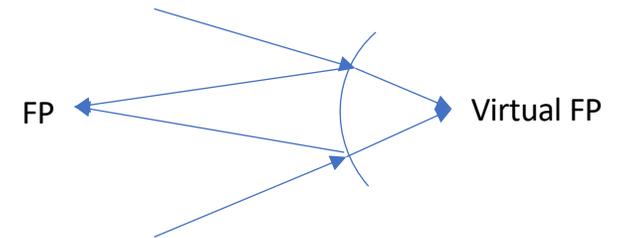


# Multiple Reflectors

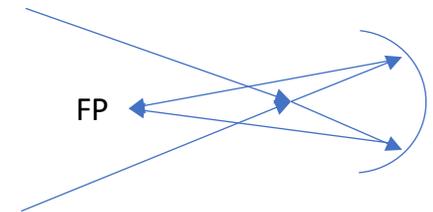
**Newtonian** – flat sub-reflector



**Cassegrain** – hyperbolic sub-reflector



**Gregorian** – elliptical sub-reflector



## Why??

- + Reduce feedline loss by moving the FP back toward the dish
- + Cassegrain and Gregorian multiply the F/D improving illumination efficiency of low F/D dishes
- - for small dishes blockage increases significantly
- - double diffraction, spillover and ohmic losses

# Example Cassegrains

18" diameter main  
2.75" diameter sub  
2.5% sub blockage  
40 GHz min

10 GHz min  
10" diameter sub  
31% sub blockage



36" diameter main  
4" diameter sub  
1.4% sub blockage  
24 GHz min

# Axially Displaced Ellipse (Gregorian)

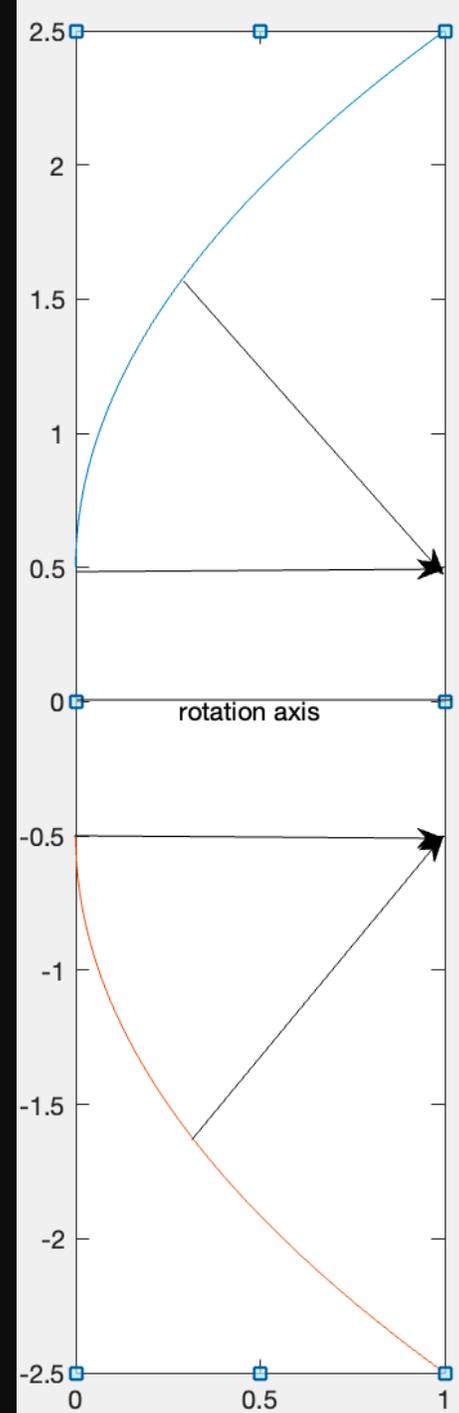
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Step 1: displace the parabola from the origin opening up a hole in the center

This creates a circular ring of focus rather than a point focus

In the example the parabola is displaced 0.5 from the origin

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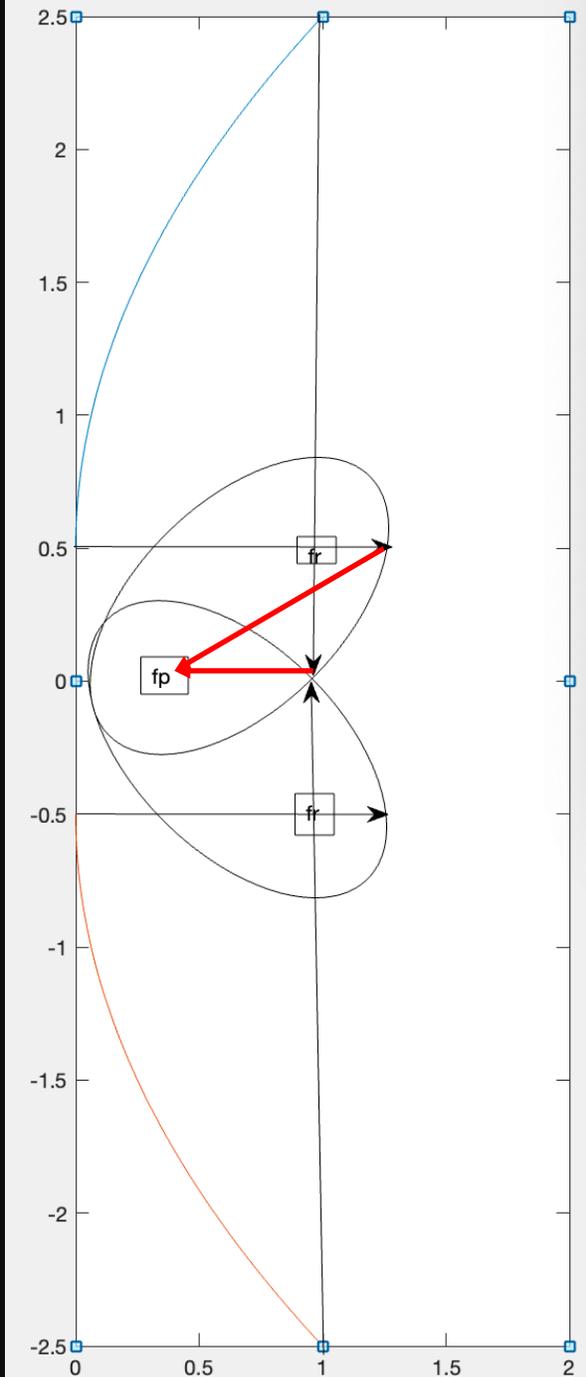


# ADE

Step 2: use a rotated tilted *ellipse* to convert the focus ring to a focus point

Note that at the focus ring the wavefronts to the inner and outer edges of the displaced parabola cross

The crossing distributes the highest energy density of the feed to the outer edges of the parabola



# Inefficiencies ADE vs. Offset

| Inefficiency | ADE     | Offset  |   |
|--------------|---------|---------|---|
| Illumination | 0.96    | 0.88    | ← |
| Spillover    | 0.96    | 0.88    | ← |
| Blockage     | 0.96    | 0.97    |   |
| Ohmic        | 0.99    | 0.99    |   |
| Surface      | 0.97    | 0.97    |   |
| Diffraction  | 0.98    | 0.98    |   |
| Feedline     | 0.98    | 0.98    |   |
|              | 82%     | 69%     |   |
|              | -0.9 db | -1.6 db |   |

# Shaped multiple reflectors

Don't have to use conic sections (Parabola, ellipse, hyperbolic) as long as the ray traced distance from the feedpoint to the planar wave is constant

Shaping the sub-reflector and the main reflector enables better energy distribution to be achieved like the ADE

Efficiencies of up to 85% have been measured

# Reflectarray

Don't have to make all the path lengths equal!!!

It's the constant phase at the plane that ensures directivity

Equal path lengths produce an in-phase wavefront at all frequencies

If we can operate narrow band other reflector structures become possible

For instance: a planar array of dipole reflectors that use passive or active phase tuning to produce an in-phase reflected wavefront

# Fresnel reflector

A Fresnel dielectric plate in front of a flat reflector can be used to generate the phase shifts needed to result in a planar wavefront

The dielectric thickness is kept low in order to minimize absorption loss

Efficiencies of  $\leq 30\%$  are typical for this type of structure

# Conclusions

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- There are a wide range of parabolic type reflector antennas with various tradeoffs:

Efficiency

Ease of construction

- Efficiencies higher than a good offset parabola while possible are less than 1 db

